

Amendments to the Claims:

This listing of claims will replace all prior versions, and listings, of claims in the application.

Listing of Claims:

Claim 1. (currently amended) A case-hardened gear which is made from a steel material comprising 0.45 to 1.5 wt% C and 0.3 to 1.5 wt% Cr, and optionally including 0.1 to 0.5 wt% V, said steel material containing cementite ((Fe, Cr)<sub>3</sub>C) dispersed therein, wherein an average Cr concentration in said cementite is 2.5 to 10 wt%, and

said gear having a rolling contact surface layer having a case-hardened layer being formed by induction heating from a temperature equal to or lower than the A1 temperature to a quenching temperature of 900 to 1100°C and subsequent cooling of said rolling contact surface layer, said case-hardened layer having a structure tempered at a low temperature of 100 to 300°C in which 2 to 18% by volume of the cementite containing solid-dissolved Cr therein is dispersed in a martensite parent phase, said martensite parent phase containing 0.25 to 0.8 wt% solid-dissolved carbon,

wherein the cementite dispersed in the rolling contact surface layer is substantially granulated and the cementite has an average particle diameter of 0.1 to 1.5  $\mu\text{m}$ .

Claim 2. (canceled)

Claim 3. (canceled)

Claim 4. (previously presented) The case-hardened gear according to claim 1, wherein the cementite dispersed in the rolling contact surface layer has at least a portion thereof in a pearlitic structure.

Claim 5. (previously presented) The case-hardened gear according to claim 1, wherein the rolling contact surface layer contains 10 to 60% by volume retained austenite.

Claim 6. (previously presented) The case-hardened gear according to claim 1, wherein said gear is made from a steel material having substantially the same composition as that of the rolling contact surface layer, the rolling contact surface layer

being subjected to induction hardening so as to have a parent phase of a martensitic structure in which prior austenite grains are refined to a size equal to or higher than ASTM grain size No. 10.

**Claim 7. (previously presented)** The case-hardened gear according to claim 1, which is made from a steel material further containing (i) 0.5 to 3.0 wt% Si, 0.25 to 1.5 wt% Al, or 0.5 to 3.0 wt% (Si + Al); and (ii) one or more alloy elements selected from the group consisting of Mn, Ni, Mo, Cu, W, B and Ca, and the balance being Fe and unavoidable impurity elements.

**Claim 8. (currently amended)** The case-hardened gear according to claim 7, wherein the steel material ~~further~~ comprises 0.3 to 1.5 wt% Ni and 0.25 to 1.5 wt% Al.

**Claim 9. (currently amended)** The case-hardened gear according to claim 1, which is made from a steel material containing at least 0.05 to 0.2 wt% in total of one or more alloy elements selected from the group consisting of Ti, Zr, Nb, Ta and

Hf, and ~~one or more compounds selected from the group consisting of the carbides [[,]] nitrides and carbonitrides~~ of said alloy elements, said ~~compounds~~ carbides having an average particle diameter of 0.1 to 5  $\mu\text{m}$  and are dispersed within the steel material, wherein the rolling contact surface layer contains 0.5 to 1.5 wt% C in said rolling contact surface layer, the rolling contact surface layer having a martensite parent phase tempered at a low temperature after quenching.

**Claim 10.. (currently amended)** The case-hardened gear according to claim 1 which has teeth, wherein there is a relationship between a DI value in inches indicating the hardenability of a martensite phase and a ~~diametral pitch~~ P gear module M, wherein ~~[[P]]~~ M is a value obtained by the ~~number of the teeth~~ pitch diameter divided by the ~~pitch diameter~~ number of teeth of said gear, which satisfies the following relationship:  
 ~~$DI \leq 0.12 \times 1/2.54 \times P + 0.2$~~   $DI \leq 0.12 \times M + 0.2$ , said martensite phase being previously a ferrite phase and containing 0.25 to 0.8 wt% solid-dissolved carbon.

**Claim 11. (previously presented)** The case-hardened gear according to claim 10, wherein said steel material further contains 0.2 to 0.5 wt% Mn, 0.5 to 2 wt% Si, 0.2 wt% or less Mo, and 0.2 wt% or less W.

**Claim 12. (previously presented)** The case-hardened gear according to claim 10, wherein said steel material contains 1.2 to 1.5 wt% C and 0.6 to 1.5 wt% Cr, and wherein said steel material further contains 0.2 to 0.5 wt% Mn, 0.5 to 2 wt% Si, 0.2 wt% or less Mo, and 0.2 wt% or less W.

**Claim 13. (previously presented)** The case-hardened gear according to claim 10, wherein a compressive residual stress of 50 kgf/mm<sup>2</sup> or more remains at least on the surfaces of the roots of the teeth.

**Claim 14. (previously presented)** The case-hardened gear according to claim 13, wherein a compressive residual stress of 50 kgf/mm<sup>2</sup> or more is allowed to remain on tooth profile surface layers each comprising a tooth top, a pitch circle position, a

tooth root and a tooth bottom, by a mechanical processing means which is shot peening for generating said compressive residual stress.

**Claim 15. (previously presented)** The case-hardened gear according to claim 13, wherein a compressive residual stress of 50 kgf/mm<sup>2</sup> or more is allowed to remain on surface layers at the ends of the teeth by a mechanical processing means which is shot peening for generating said compressive residual stress.

**Claim 16. (canceled)**

**Claim 17. (previously presented)** A method of producing a case-hardened gear from a steel material containing 0.45 to 1.5 wt% C and 0.3 to 1.5 wt% Cr, and optionally including 0.1 to 0.5 wt% V, the method comprising:

(a) a Cr concentration treatment step for heating the steel material at 300°C to the A1 temperature in a two phase (cementite + ferrite) region such that an average Cr concentration of cementite dispersed in the steel material is 2.5 to 10 wt%;

(b) an induction hardening treatment step for induction heating the steel material from a temperature equal to or lower than the A1 temperature to a quenching temperature of 900 to 1100°C within 10 seconds, followed by rapid cooling; and

(c) a tempering treatment step for heating the steel material to 100 to 300°C.

Claim 18. (canceled)

Claim 19. (canceled)

Claim 20. (currently amended) The method of producing a case-hardened gear according to claim 17, ~~which further comprises a preheating treatment step in which the steel material is preheated at 300°C to the A1 temperature before the induction hardening treatment step~~ [[,]] and wherein the speed of heating from a temperature equal to or lower than the A1 temperature to a quenching temperature of 900 to 1100°C in the induction hardening treatment step is set to 150°C/sec or more.

Claim 21. (canceled)

**Claim 22. (previously presented)** The method of producing a case-hardened gear according to claim 17, further comprising a mechanical treatment step in which a compressive residual stress of 50 kgf/mm<sup>2</sup> or more is generated by a treatment which is shot peening, in a part or the whole of the rolling contact surface layer of the gear after the induction hardening treatment step.

**Claim 23. (previously presented)** The case-hardened gear according to claim 1, wherein the steel material includes 0.1 to 0.5 wt% V.

**Claim 24. (previously presented)** The method of producing a case-hardened gear according to claim 17, wherein the steel material includes 0.1 to 0.5 wt% V.

**Claim 25. (previously presented)** A method of producing a case-hardened gear from a steel material containing 0.8 to 1.5 wt% C and 0.3 to 1.5 wt% Cr, and optionally including 0.1 to 0.5 wt% V, the method comprising:

(a) a Cr concentration treatment step for heating the steel material at the A1 temperature to 900°C in a two phase (cementite



+ austenite) region such that an average Cr concentration of cementite dispersed in the steel material is 2.5 to 10 wt%;

(b) an induction hardening treatment step for induction heating the steel material from a temperature equal to or lower than the A1 temperature to a quenching temperature of 900 to 1100°C within 10 seconds, followed by rapid cooling; and

(c) a tempering treatment step for heating the steel material to 100 to 300°C.

**Claim 26. (previously presented)** The method of producing a case-hardened gear according to claim 25, which further comprises carrying out a spheroidizing treatment step after the Cr concentration treatment step, wherein in the spheroidizing treatment step, granular cementite having an average particle diameter of 0.1 to 1.5  $\mu\text{m}$  is dispersed by cooling to a temperature lower than the A1 temperature and then reheating to a temperature equal to or higher than the A1 temperature.

**Claim 27. (previously presented)** The method of producing a case-hardened gear according to claim 25, which further comprises

a preheating treatment step in which the steel material is preheated at 300°C to the A1 temperature before the induction hardening treatment step, and wherein the speed of heating from a temperature equal to or lower than the A1 temperature to a quenching temperature of 900 to 1100°C in the induction hardening treatment step is set to 150°C/sec or more.

**Claim 28. (previously presented)** The method of producing a case-hardened gear according to claim 25, further comprising a mechanical treatment step in which a compressive residual stress of 50 kgf/mm<sup>2</sup> or more is generated by a treatment which is shot peening, in a part or the whole of the rolling contact surface layer of the gear after the induction hardening treatment step.

**Claim 29. (previously presented)** The method of producing a case-hardened gear according to claim 25, wherein the steel material includes 0.1 to 0.5 wt% V.